

PATENT SPECIFICATION (11) 1 504 873

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(54) ELECTROMAGNETIC DEVICES

(71) We, SIMMS GROUP RESEARCH & DEVELOPMENT LIMITED, a British Company, of Well Street, Birmingham B19 2XF, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

This invention relates to electromagnetic devices comprising a pair of relatively movable magnetisable members and a winding or windings through which electric current can be passed to produce a magnetic field to effect relative movement of the members.

The object of the invention is to provide such a device in a simple and convenient form.

According to the invention an electromagnetic device comprises a pair of magnetisable members, one of said members having a face in which is defined a plurality of slots disposed in side by side relationship, the other of said members having a face on which is formed a plurality of projections disposed in side by side relationship, said projections having a width which is smaller than the width of the slots, said members being positioned relative to each other such that the projections enter into the slots, the initial relative position of the members being such that the projections are disposed off centre in the respective slots and the two members being relatively movable in the direction such that each projection can move from one side to the other side of the respective slot, some or all of said slots accommodating an electrical winding, the connection of the winding or windings being such that any two slots in which the flow of current in the windings therein is in the same direction are separated by a slot with either no winding therein or a winding in which the flow of current is in the opposite direction, the arrangement being such that when the winding or windings is/are energised a magnetic field is produced and the members will be urged relative to each other from said initial position in a direction to reduce the size of the smaller of the gaps defined between the side

faces of the slots and the side walls of the respective projections.

According to another aspect of the invention an electromagnetic device comprises a pair of magnetisable members, one of said members having a face in which is defined a plurality of slots disposed in side by side relationship, the other of said members having a face on which is formed a plurality of projections disposed in side by side relationship, said projections having a width and a depth which are smaller than the width and the depth of the slots, said members being positioned relative to each other such that the projections enter into said slots, the initial relative position of the members being such that the projections are disposed off centre in the respective slots and the two members being relatively movable in the direction such that each projection can move from one side to the other side of the respective slot, each of said slots accommodating an electrical winding, the connections of the windings being such that the flow of electric current in the windings in adjacent slots will be in opposite directions, the arrangement being such that when the windings are energised a magnetic field is produced and the members will be urged relative to each other from said initial position in a direction to reduce the size of the smaller of the gaps defined between the side faces of the slots and the side walls of the respective projections.

One example of an electromagnetic device in accordance with the invention will now be described with reference to the accompanying drawings, in which:—

Figure 1 is a sectional side elevation of the device.

Figure 2 is an enlarged section of a portion of the device seen in Figure 1.

Figures 3, 4, 5 and 6 are views similar to Figure 2 and show alternative arrangements of the device of Figure 1.

Figure 7 shows a further modification of the device, and

Figure 8 shows a further arrangement of the device.

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The design requirements for the device include a low inertia of the moving parts, a high mechanical force output and high speed operation.

5 With reference now to Figures 1 and 2 of the drawings the device comprises a central core member 10 which at one end is provided with a threaded stud whereby it can be secured to a support member 11. Disposed between the core member and the support member 11 is a cup shaped part 12 through an aperture in the base wall of which extends the stud. The cup shaped part 12 acts to provide radial location of an annular member 13 about the core member 10, whilst at the same time allowing relative axial movement of the members. At the opposite end a sleeve 12a provides radial location of the two members whilst at the same time allowing relative axial movement.

20 The core member 10 and the annular member 13 are formed from magnetizable material. Moreover, the core member 10 is provided with slots into which enter projections formed on the annular member. In practice, and as shown, the members are provided with interengageable screw threads, the threads being formed so that appreciable relative axial movement can take place between the members. For reasons which will be explained, the threads formed on the members are two start threads although it will be understood that any multiple of two threads may be used. It will be seen that the core member 10 in the case of a two start thread, is provided with two helical slots 14, 15 whilst the annular member 13 is provided with two helical projections 16, 17 disposed in the slots 14, 15 respectively. In the example of Figures 1 and 2 the threads on the two members are of identical cross section. This is not essential as will be seen in the remaining figures. It is nevertheless convenient for the purpose of description to talk about slots and projections and the use of the term slot will be confined to the threads on the member upon which windings are wound.

50 As shown in Figures 1 and 2 each slot 14, 15 in the core member 10 is provided with a winding 18, 19 in this case a winding having a single turn. For the purpose of understanding, in Figure 1 the dot and cross indication is used to represent the respective windings and in Figure 2 whilst indicating the respective windings, the dot and cross indication also indicates the direction of electric current flow. The two windings 18, 19 are formed from a continuous length of insulated wire which is wound away from one end of the core member 10 conveniently the stud end of the core member, along one thread through a transverse aperture 20 at the other end of the core member and back along the other

thread towards said one end of the core member.

The shape of the threads formed on the two members is important. The projections 16, 17 have radially extending side faces 21 which in the de-energised condition of the winding are disposed in spaced parallel side by side relationship to side faces 22 defined by the slots. The other faces 23 of the projections 16, 17 incline outwardly and the other faces 24 of the slots incline in a similar manner. The axial spacing between the faces 24, 23 is considerably larger than the spacing between the faces 21, 22.

80 When electric current is passed through the wire, each winding 18, 19 produces a magnetic flux which follows a path through the core member 10 across the two gaps defined between the faces 21 and 22 and through the member 13. The two members therefore strive to move relative to each other to reduce the size and reluctance of the gaps and a mechanical force is created. It will be noted that because of the different direction of the windings 18, 19 the direction of the flux generated due to each winding is opposite. However, for any one of said gaps the direction of the flux flowing across the gap due to the two windings, is the same. The flux generated by the two windings therefore has an additive effect. The path for leakage flux for instance between the faces 23, 24 is maintained as large as possible by suitable choice of the configuration of the threads and by the pitch of the threads.

In the arrangement shown in Figure 3 each winding is provided with two turns and these may be connected in parallel or in series. If the series arrangement is desired a single length of wire may be used for both windings. Figure 3 also demonstrates the point made earlier namely that the threads on the two members need not be of identical cross section. With the arrangement shown in Figure 3 there may be more leakage of flux due to the shorter gaps between the various faces.

115 In the arrangement which is shown in Figure 4 the annular member 25 has been made lighter by trimming away all surplus material so that the member is as light as possible so as to reduce its inertia. Material can be removed in this fashion because in practice the flux does not penetrate very far into the magnetisable material. However, in order to produce a high mechanical force the flux density across the gaps between the faces 21, 22 should be as high as possible and therefore the flux should penetrate the material as much as possible. The flux penetration depends on the type of material, the amplitude of the flux and also the rate of change of flux. In conventional devices of this type, laminated materials are

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often used to achieve greater flux penetration. This is not necessary with the present design even with a high flux density and with high rates of change of flux providing a suitable material is chosen. Such a material would have a high electrical resistivity and a low magnetic permeability such as a sintered pure iron for example that sold under the name "Hoganas". An alternative material would be a linear ferrite material.

The arrangement shown in Figure 5 also uses as thin an annular member 26 as possible. Moreover, the slots in the core member are as small as possible and are more or less completely filled with copper. The flux path is also as small as possible but it is to be noted that the gaps between the faces of the projections and slots are inclined and therefore the axial force acting to move the members in a relative axial direction will be reduced. Furthermore, the location of the core member 10 and the annular member 26 is rather critical because of the proximity of the windings to the projections and because of the smaller clearances employed in the construction.

The arrangement shown in Figure 6 is in many respects similar to the arrangement shown in Figure 2 with the annular member modified as shown in Figure 4. In addition, each winding is provided with four turns.

In the arrangement shown in Figure 7 each slot is provided with a pair of windings 27, 28. The winding 27 can be energised before the winding 28 so as to provide a steady base flux. This base flux would not in practice be of sufficient magnitude to cause movement of the part actuated by the device, but would effect partial saturation of the material forming the core and annular members. When movement of the part is required the current is supplied through the winding 28 and because of the lower effective permeability of the material the depth of penetration of the flux is higher thereby leading to a high flux density in the gaps.

In the examples described the slots including the windings have been formed in the core member. It will be understood, however, that the slots and windings could have been formed in the annular member. In Figure 8 there is shown an example in which slots are formed on the internal periphery of an annular member 29. In this case, however, there is also a core member 10 and disposed between these members is a movable member 30 having the projections formed thereon and which are positioned in the respective slots of the members 10 and 29.

In each of the examples described, the flux penetration may be increased by cutting axial slots along the peripheral surfaces of both the core member and annular member.

In each of the examples described each slot as defined by a thread groove is provided with a winding. It is possible, however, to provide a single winding in one only of the thread grooves. Moreover, in the case of a multiple of two start threads, two of the thread grooves may be provided with windings and if the current in the windings is in the same direction then there must be an empty thread groove disposed therebetween. If on the other hand the flow of current in the two windings is in the opposite direction, then the grooves accommodating the windings must be adjacent each other.

In each of the examples described the helical air gaps across which the axial pulling force is developed are equal. When the gaps are reduced to zero upon relative axial movement of the members there is the risk that the faces defining the gaps will stick to each other due to the action of residual magnetism. The resulting holding force can be reduced by machining the members such that the faces defining one gap only can move into contact with each other.

Moreover, the devices described are single acting only. That is to say the members forming the device move relatively to each other in one direction only when the winding is energised. A double acting effect can be obtained by providing two such devices as described in back to back relationship. In this case the winding of one device would be energised to achieve relative movement in one direction and the winding of the other device to achieve movement in the opposite direction.

In the case of the device shown in Figure 8 it is possible to achieve the double acting effect by a comparatively simple modification. It should be noted however that the two windings are then energised separately to achieve the two directions of movement. The modification is to dispose the projections on one side of the member 30 on the opposite side of the ribs of the adjacent member 10 or 29.

In the devices described since the projections and slots are helically disposed, in addition to the axial force which is generated upon energisation of the winding there will also be a turning force. The magnitude of this force will depend upon the helix angle and the members must be mounted so as to resist this force. The turning force can however be balanced by providing a further device having the opposite helix angle but arranged to pull in the same axial direction when the winding is energised.

The devices described have employed a member 10 of solid form. It is advantageous for the member 10 to be of tubular form with the wall thickness as small as possible. The actual thickness of the wall being suffi-

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		cient to transmit the magnetic flux. In this manner eddy current loss in the member 10 can be reduced.	
5	WHAT WE CLAIM IS:—		
10	1. An electromagnetic device comprises a pair of magnetisable members, one of said members having a face in which is defined a plurality of slots disposed in side by side relationship, the other of said members having a face on which is formed a plurality of projections disposed in side by side relationship, said projections having a width which is smaller than the width of the slots, said members being positioned relative to each other such that the projections enter into the slots, the initial relative position of the members being such that the projections are disposed off centre in the respective slots and the two members being relatively movable in the direction such that each projection can move from one side to the other side of the respective slot, some or all of said slots accommodating an electrical winding, the connection of the winding or windings being such that any two slots in which the flow of current in the windings therein is in the same direction are separated by a slot with either no winding there-in or a winding in which the flow of current is in the opposite direction, the arrangement being such that when the winding or windings is/are energised a magnetic field is produced and the members will be urged relative to each other from said initial position in a direction to reduce the size of the smaller of the gaps defined between the side faces of the slots and the side walls of the respective projections.	70	
15	2. An electromagnetic device comprises a pair of magnetisable members, one of said members having a face in which is defined a plurality of slots disposed in side by side relationship, the other of said members having a face on which is formed a plurality of projections disposed in side by side relationship, said projections having a width and a depth which are smaller than the width and the depth of the slots, said members being positioned relative to each other such that the projections enter into said slots, the initial relative position of the members being such that the projections are disposed off centre in the respective slots and the two members being relatively movable in the direction such that each projection can move from one side to the other side of the respective slot, each of said slots accommodating an electrical winding, the connections of the windings being such that the flow of electric current in the windings in adjacent slots will be in opposite directions, the arrangement being such that when the windings are energised a magnetic field is produced and the	75	
20		members will be urged relative to each other from said initial position in a direction to reduce the size of the gaps defined between the side faces of the slots and the side walls of the respective projections.	70
25		3. A device according to claim 1 or claim 2 in which the depth and shape of the slots is such in relation to the size of the projections as to provide accommodation for the windings.	75
30		4. A device according to claim 2 in which one of said members is of cylindrical form and the other member is of annular form, said one member being located within the other member, said slots and projections being defined by screw threads formed on the inner surface of the other member and the outer surface of the one member.	80
35		5. A device according to claim 4 in which the screw threads are two or a multiple of two, start threads, said windings being connected such that the current flow in the windings in alternate thread grooves is in one direction and the current flow in the other thread grooves is in the opposite direction.	85
40		6. A device according to claim 5 in which said windings comprise a single length of wire.	90
45		7. A device according to claim 6 in which said wire is wound along one groove towards one end of the member and is returned along an adjacent groove towards the other end of the member.	95
50		8. A device according to claim 7 in which said wire passes through an aperture formed in the member in which the grooves are formed.	100
55		9. A device as claimed in claim 7 in which a plurality of turns are provided in each groove.	105
60		10. A device as claimed in claim 5 in which each groove is provided with a pair of windings one of which can be energised to partly magnetize the members and the other of which can be energised to magnetize the members a further amount to cause relative movement of the members.	110
65		11. A device according to claim 4 in which said other member is machined on its outer periphery to reduce the thickness of material and thereby reduce the inertia of the member.	115
		12. A device according to claim 4 in which said other member is provided with projections on its outer peripheral surface and a further annular member is provided surrounding said other member, said further annular member having helical slots machined on its internal periphery in register with projections on the outer surface of said other member, the helical slots in said further member also being provided with windings.	120
		13. A device as claimed in claim 12 in	125
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which the windings on said one and said further members when energised effect movement of said other member in the same direction.

5 14. A device as claimed in claim 12 in which the windings on said one and said further members when energised effect movement of said other member in opposite directions respectively.

10 15. The combination of a pair of devices as claimed in claim 5 in which the respective members are coupled together whereby energisation of the electrical windings of one of the devices will result in relative axial movement of the members in one direction and energisation of the windings of the other of the devices will result in relative axial movement of the members in the opposite direction.

20 16. The combination of a pair of devices as claimed in claim 5 in which the respective members are coupled together, the helix angles of the projections and grooves of one of the devices being opposite to those of the other device whereby the turning force generated between the members of each device when the windings are energised is cancelled.

25 17. An electromagnetic device substantially as hereinbefore described with re-

ference to Figures 1 and 2 of the accompanying drawings.

18. An electromagnetic device substantially as hereinbefore described with reference to Figure 1 as modified by Figure 3 of the accompanying drawings. 35

19. An electromagnetic device substantially as hereinbefore described with reference to Figure 1 as modified by Figure 4 of the accompanying drawings. 40

20. An electromagnetic device substantially as hereinbefore described with reference to Figure 1 as modified by Figure 5 of the accompanying drawings.

21. An electromagnetic device substantially as hereinbefore described with reference to Figure 1 as modified by Figure 6 of the accompanying drawings. 45

22. An electromagnetic device substantially as hereinbefore described with reference to Figure 1 as modified by Figure 7 of the accompanying drawings. 50

23. An electromagnetic device substantially as hereinbefore described with reference to Figure 8 of the accompanying drawings. 55

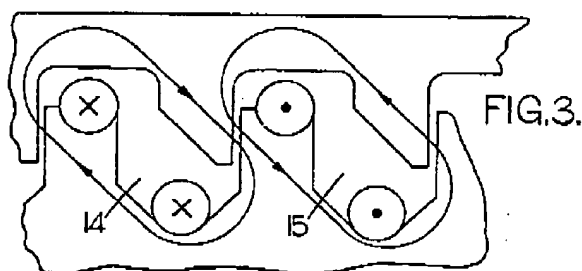
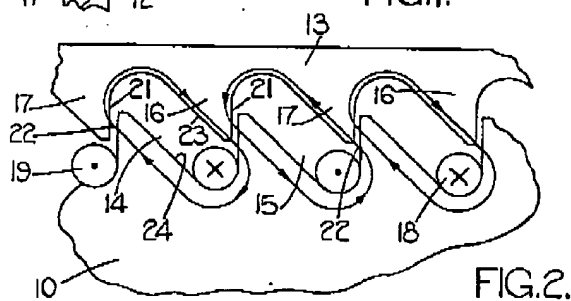
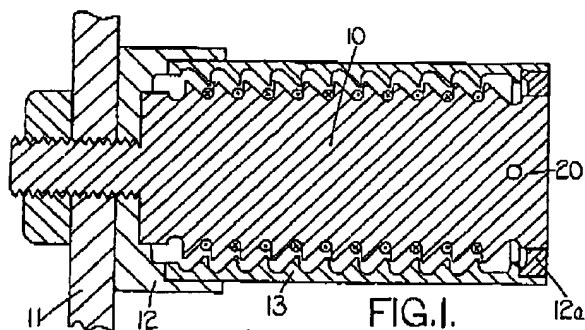
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